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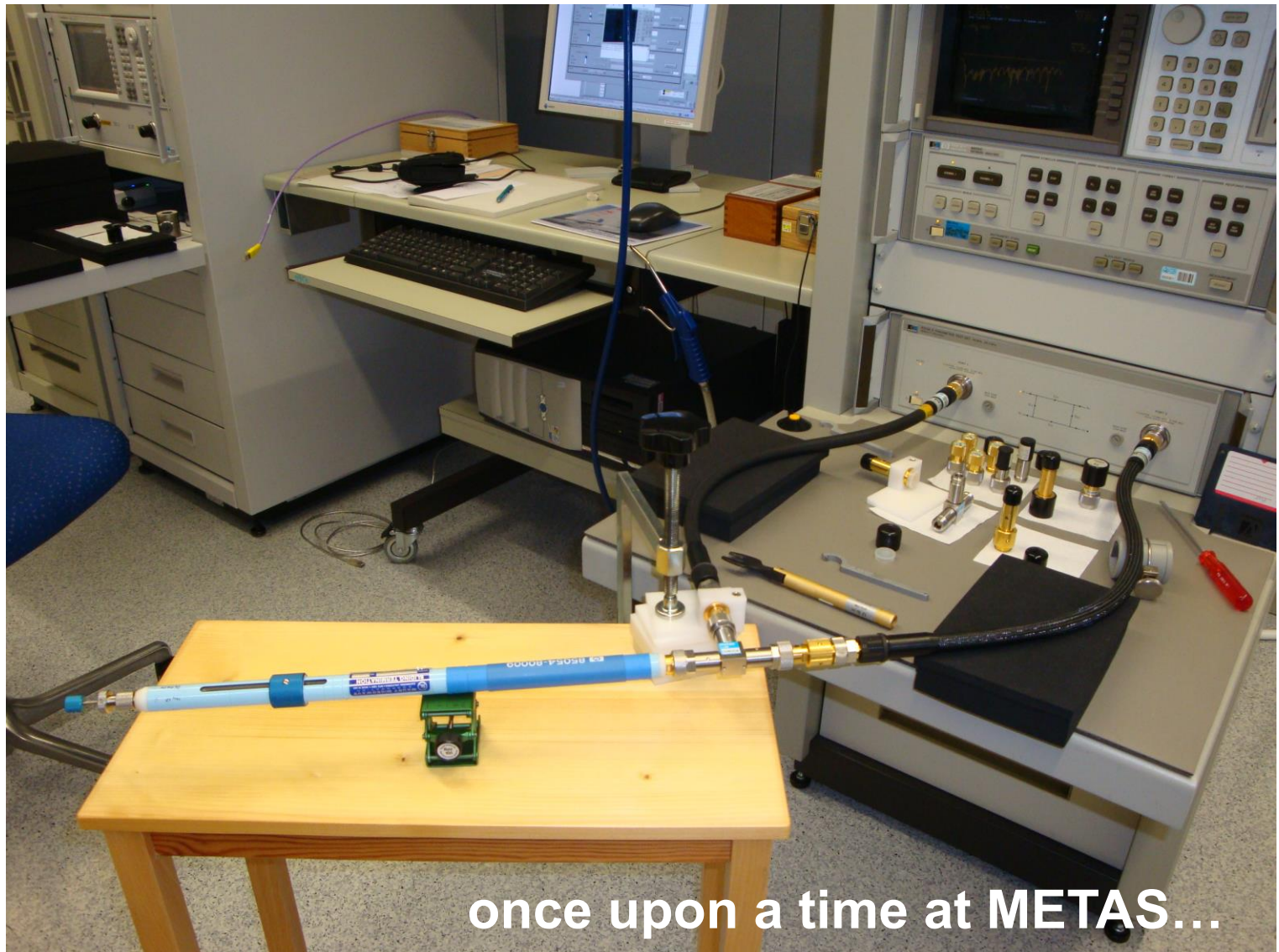
Federal Institute of Metrology METAS



# Practical hints: splitter characterization

J. Ruefenacht, M. Wollensack, J. Hoffmann, M. Zeier

# Motivation



once upon a time at METAS...

# Agenda

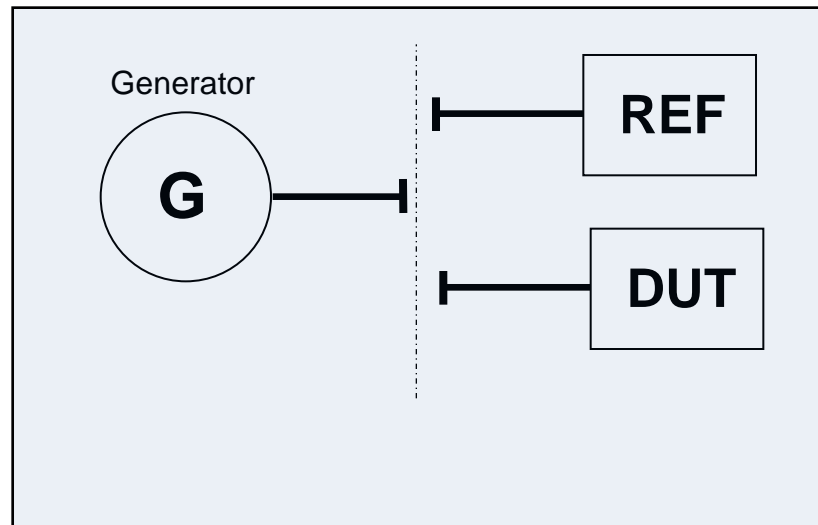
- 1. Power splitter or divider (choose the right one...)**
- 2. 2-resistor power splitter (ratio method)**
- 3. Measurement restrictions we had in our laboratory**
- 4. Power splitter measurement techniques used in the past**
- 5. How to identify a stability issue of a power splitter?**
- 6. Actual splitter measurement methods used at METAS**
- 7. Conclusions**



# Power splitter or divider

-> choose the right one...

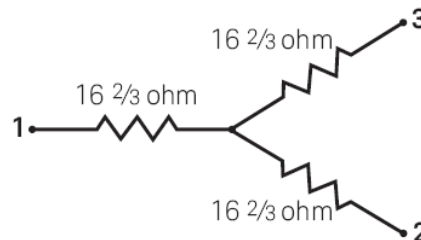
## How to divide the generator signal equally?



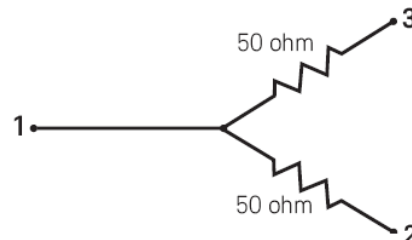
# Power divider and splitter

-> choose the right one (list not complete)

- 3-resistor power divider ( $3 * 16.7 \Omega$ ):** good match from DC to GHz, ideal e.g. for pulse signal / oscilloscope – applications, very high bandwidth, low power applications. Can be used as power combiner.

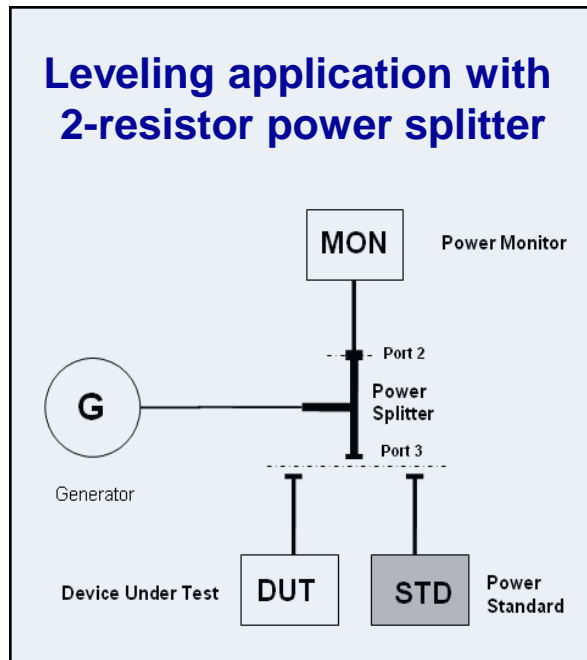


- 2-resistor splitters ( $2 * 50 \Omega$ ):** mainly used for ratio measurements and leveling loop applications, low Equivalent Source Match ( $\Gamma_{Eq}$ ), very high bandwidth, low power applications. Only the input port has  $50 \Omega$  resistance the other two ports have  $83.33 \Omega$  resistance.



# 2-resistor power splitter

## Equivalent Source Match $\Gamma_{Eq}$



- **Leveled system, can be active (ALC) or passive -> ratio method required:**  
Ratio measurements between the two output arms of the 2-resistor splitter.
- **The equivalent source match (e.g. Port 3) depends only on the S-parameters of the 2-resistor power splitter.**

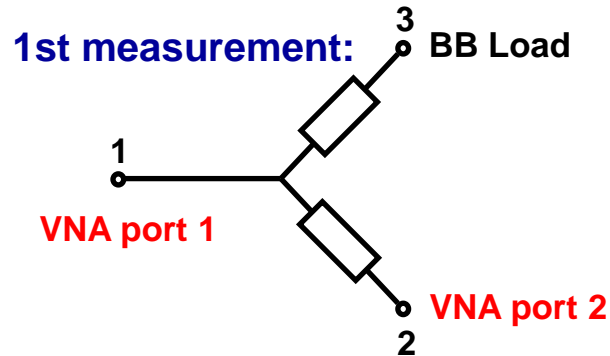
$$\Gamma_{Eq3} = S_{33} - \frac{S_{23}S_{31}}{S_{21}}$$

## 2-resistor power splitter measurement technique restrictions we had in our laboratory (to determine the equivalent source match or the tracking terms)

- Only 2-port VNA available in the past.
- An **ideal load** is needed to terminate the third splitter port.
- No data base standard definitions available (ideal 50 ohm).
- Broad band load or combination of a fixed and sliding load (circle fitting over all four S-parameters).
- Splitter with a non-insertable connector setup (e.g. 3 x female).
- Using the swap equal adapters method (uncertainties?).
- Unknown Thru not working accurately (Open, Short definitions: issue with the cal standard traceability - badly defined reference planes due to ignoring the systematic connector effects).
- Increased cable effects due to the large cable flexure.

# Russell A. Johnson method

Russell A. Johnson (hp), „Understanding Microwave Power Splitters“, Microwave Journal, December 1975



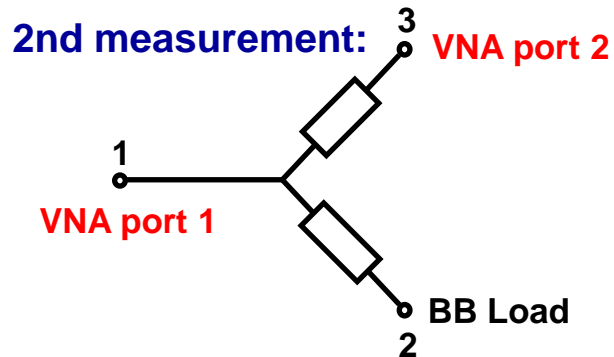
S11 -> S11  
 S21 -> S21  
 S12 ->  
 S22 -> S22

## 2-resistor splitter:

$$\Gamma_{Eq2} = S_{22} - \frac{S_{32}S_{21}}{S_{31}}$$

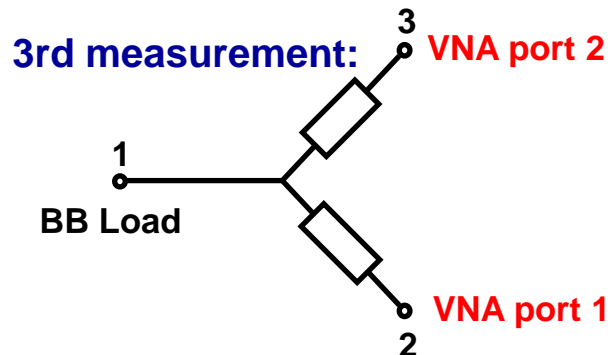
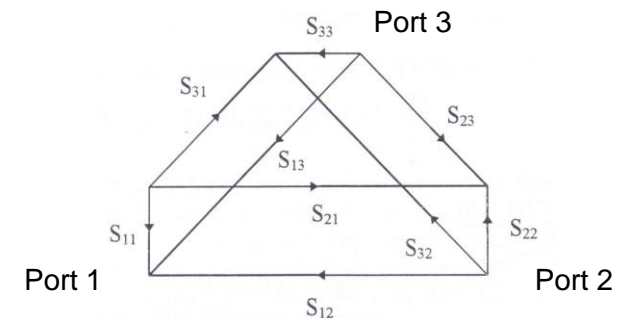
$$\Gamma_{Eq3} = S_{33} - \frac{S_{23}S_{31}}{S_{21}}$$

$$Tracking = \frac{S_{21}}{S_{31}}$$



S11 ->  
 S21 -> S31  
 S12 ->  
 S22 -> S33

## Three port device flow-graph:

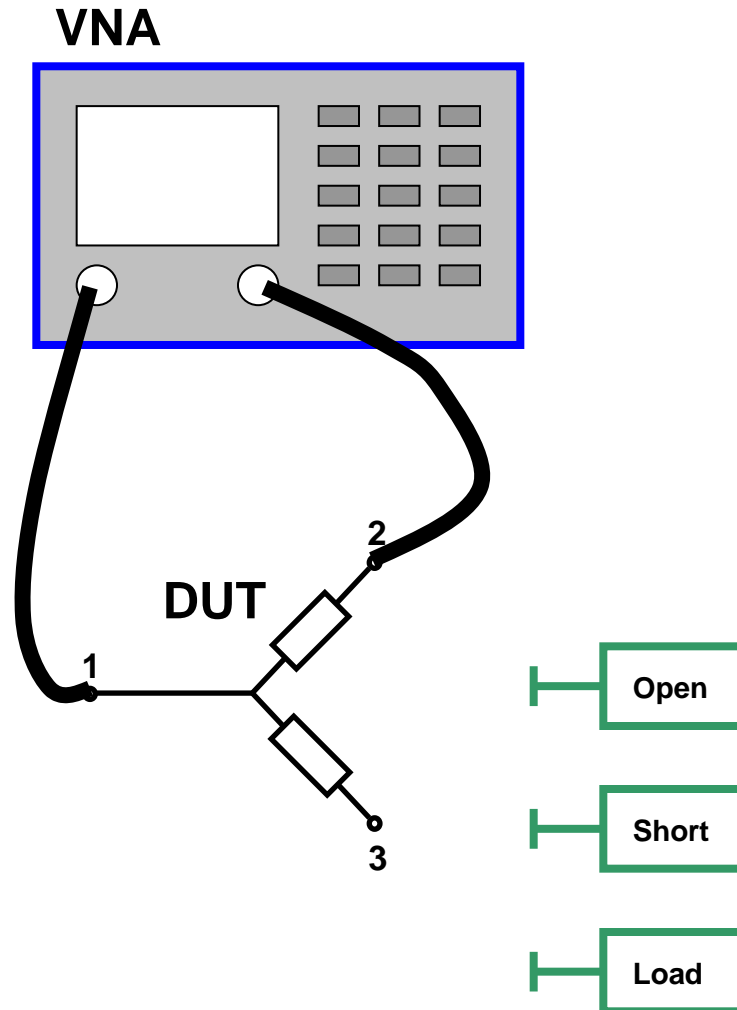


S11 ->  
 S21 -> S32  
 S12 -> S23  
 S22 ->



# Juroshek method (2-port VNA but OnePort cal)

John R. Juroshek, „A direct calibration method for measuring equivalent source mismatch“, Microwave Journal, October 1997



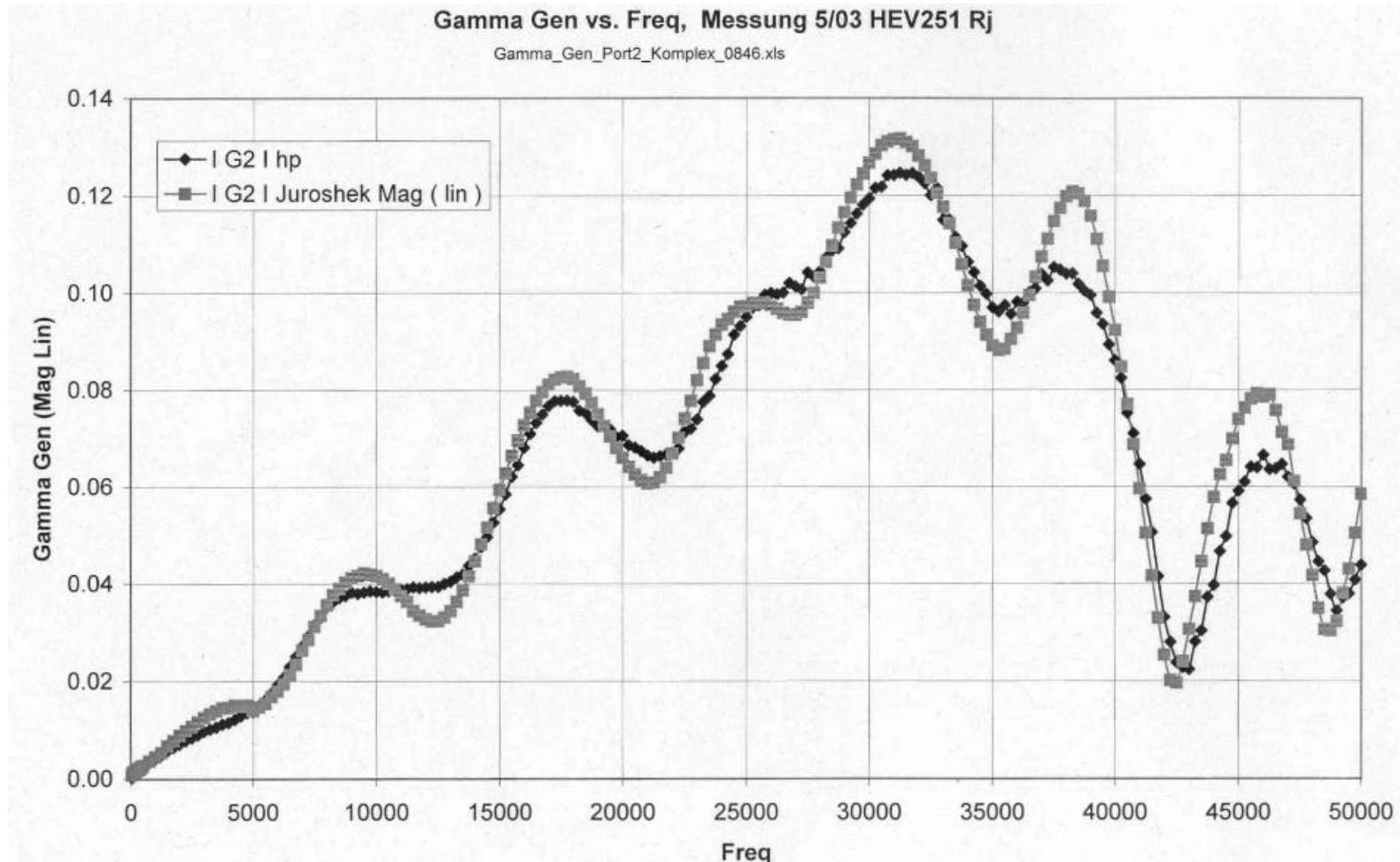
- Perform a OnePort calibration using the converted S-parameters

$$J_{33} = \frac{S_{11}}{S_{21}}$$

- Equivalent source match  $\Gamma_{Eq3}$ :  
-> equals the VNA source match

# Comparison: Russell Johnson (hp) vs Juroshek

Example: 11667C, 2.4 mm(f) splitter measurements done in 2004

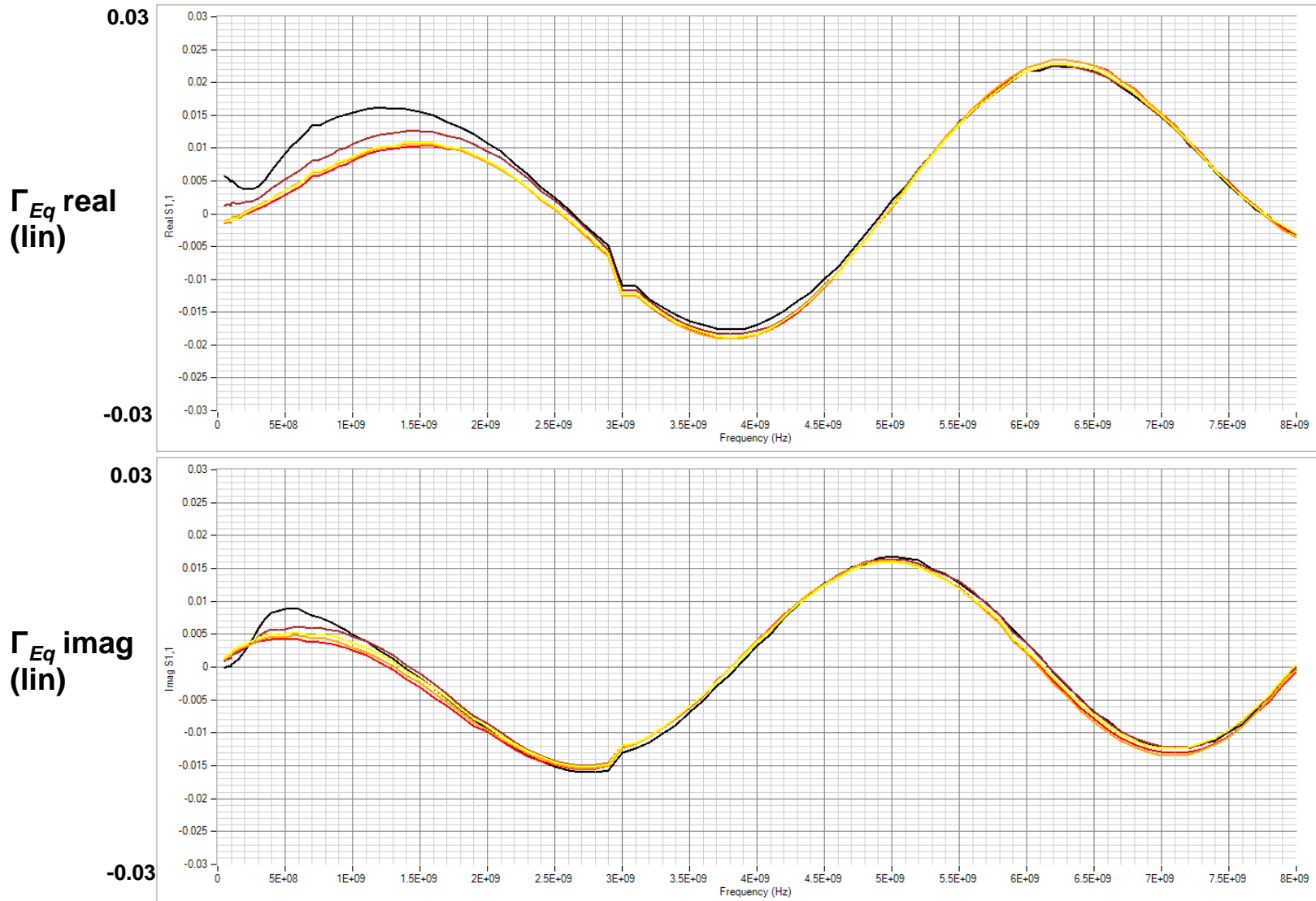


## Some typical splitter stability issues

- Pin-depth values do change after each connection:
  - centre conductors are not fixed.
  - bead structure loose.
- The center conductors are badly contacted to the splitter circuitry.
- Showing a bad long term stability (option: whit heat cycling -> burn-in)
- Resulting effect after reconnecting the cal standards:  
**The S-parameters of the splitter change during each of the performed characterisation measurements!**



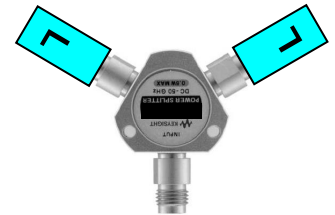
# Type-N splitter stability issue (instable $\Gamma_{Eq}$ )



# Power splitter stability pre-check

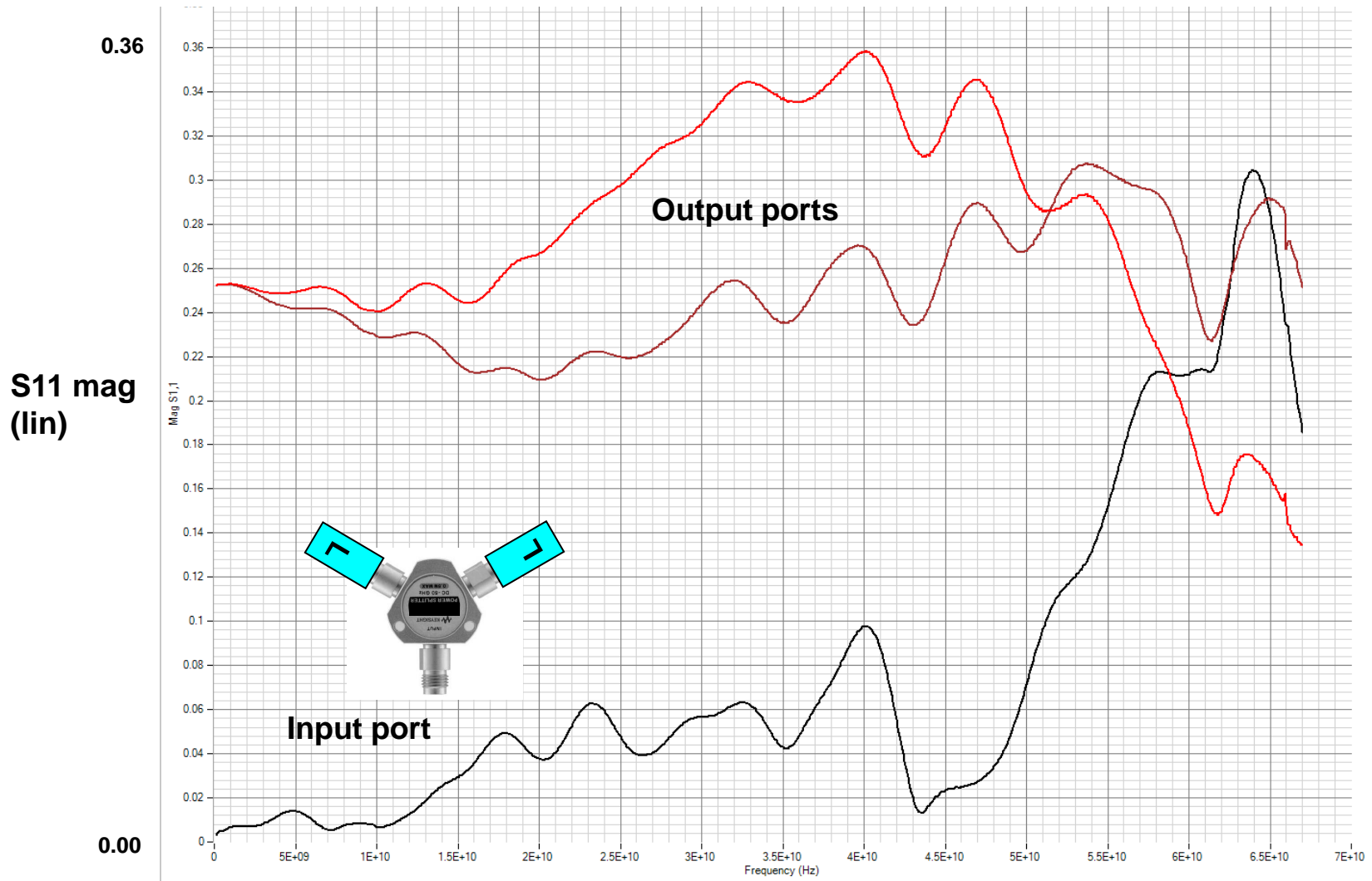
## S11 measurements at different connector orientations

- No VNA calibration needed: just measure the raw data.
- Connect two loads (or shorts) to port 2 and port 3 of the splitter.
- Measure S11 from port 1 of the splitter at different connector orientations.
- Normalize the collected data to its mean value.
- Repeat the same process for all three splitter ports.
- **optional:** use a calibrated VNA for absolute measurements.



# 1.85 mm splitter stability pre-check

measuring S11 of each port (others terminated with 50  $\Omega$ ), using a calibrated VNA



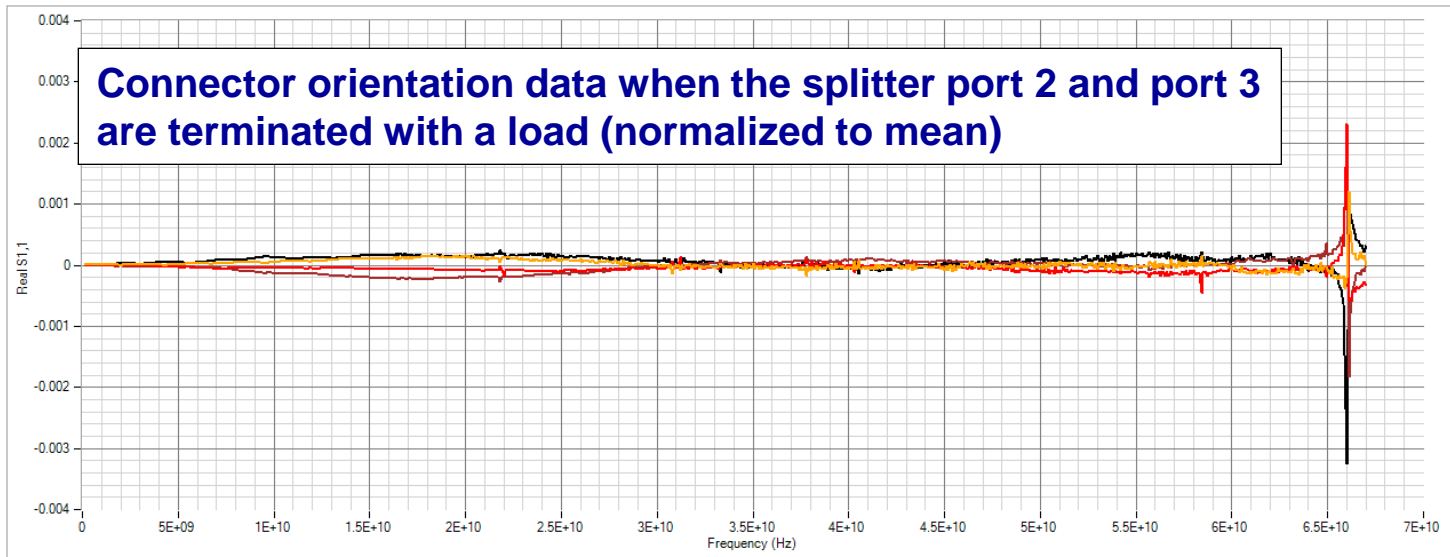


# 1.85 mm splitter stability pre-check (on port 1)

0.004

**S11 real (lin)**

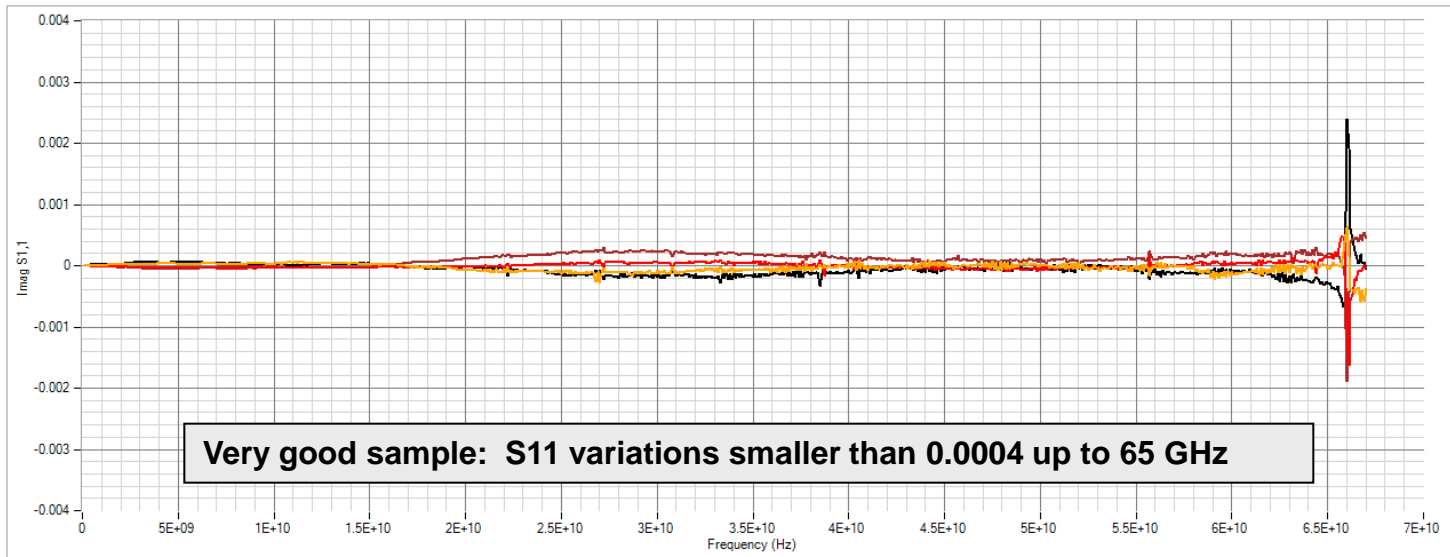
-0.004



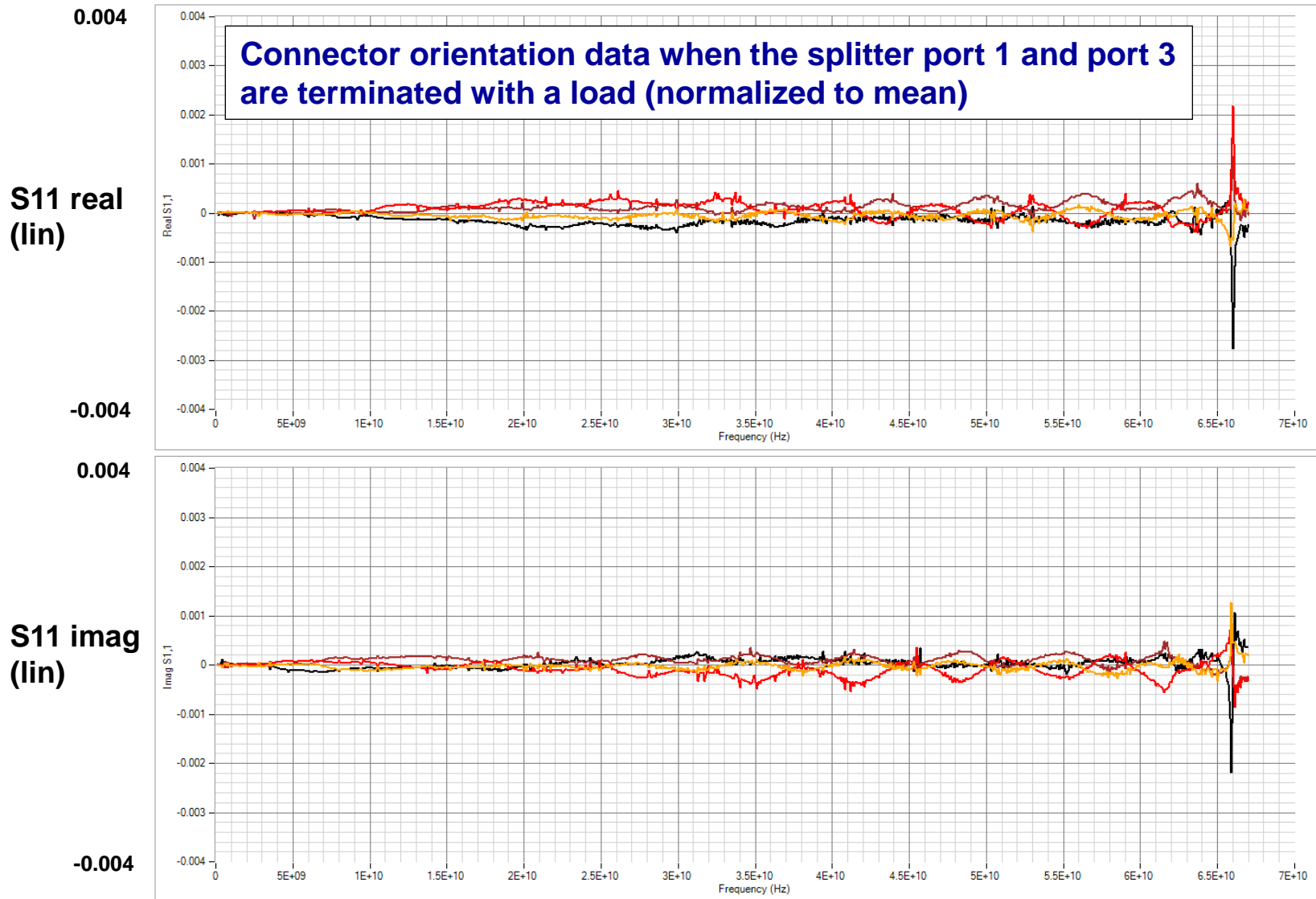
0.004

**S11 imag (lin)**

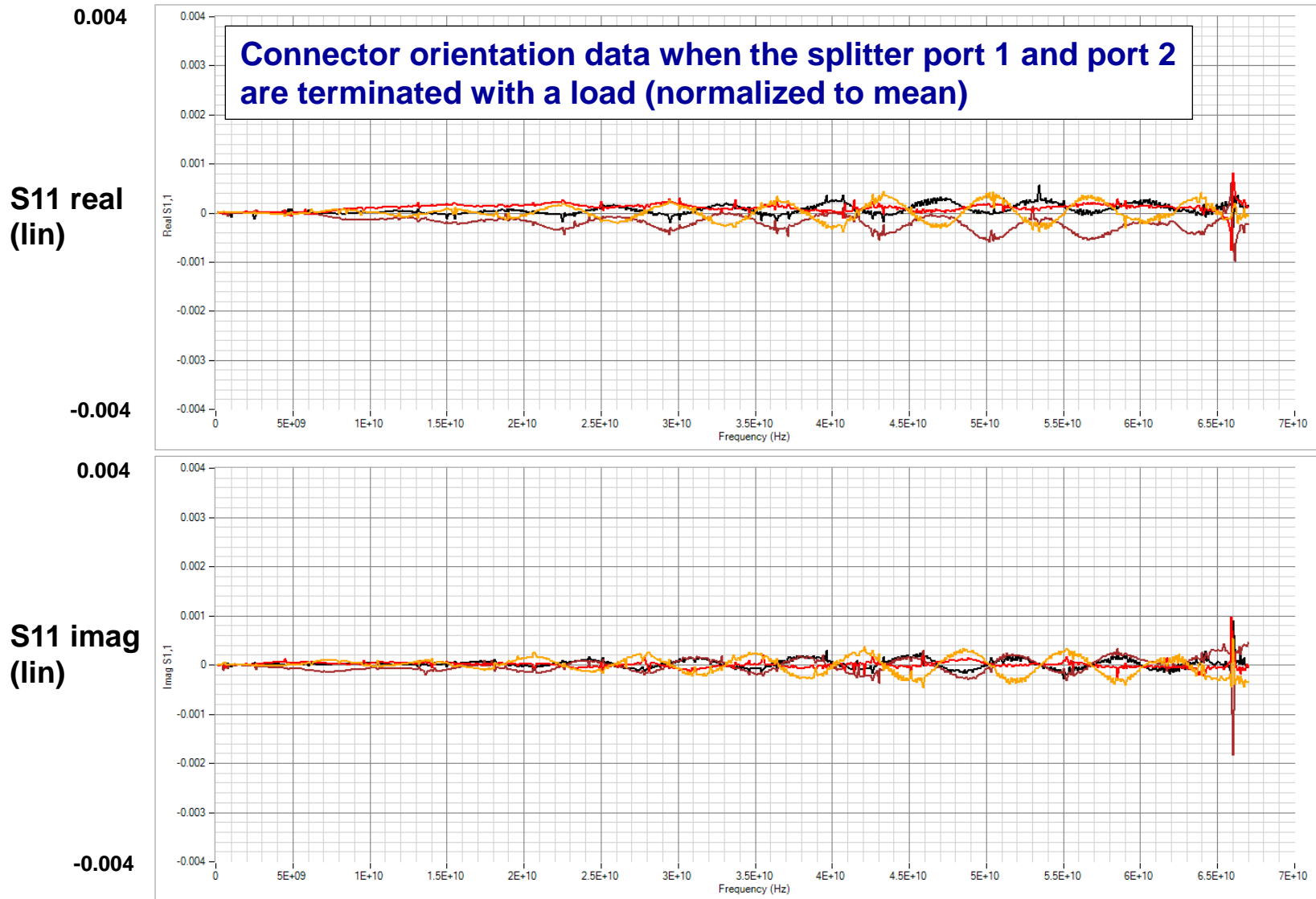
-0.004



# 1.85 mm splitter stability pre-check (on port 2)



# 1.85 mm splitter stability pre-check (on port 3)



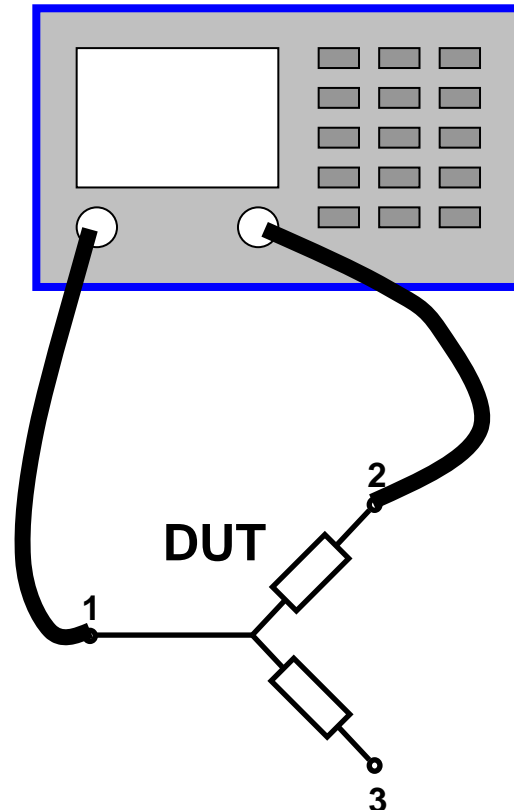
## Actual used splitter measurement methods

- **Currently preferred method at METAS (1st priority: “Palmer”):**  
**2-Port method** measuring a Load and Short on the input port
  - Rather easy and straight forward measurement setup.
  - Load and Short must **not be known** (connected to the splitter input port).
  - Requires at least 10 connections.
  - $\Gamma_{Eq}$  mainly dependent on the used load calibration standard definitions.
- **2nd priority method:**  
**Direct 3-Port** measurement method using a 4-port VNA
  - More demanding test port cable layout.
  - Requires at least 12 connections.
  - $\Gamma_{Eq}$  mainly dependent on the used load calibration standard definitions.
- **3rd priority method:**  
**Juroshok** measurement method using a 2-port VNA
  - Demanding VNA performance needs (directivity, linearity and noise).
  - Easy and straight forward measurement setup.
  - Requires at 5 connections (10 connections for  $\Gamma_{Eq}$  of both splitter ports).
  - $\Gamma_{Eq}$  mainly dependent on the used Open and Short cal standard definitions.

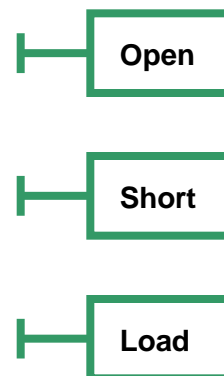
# Juroshek method (2-port VNA but OnePort cal)

John R. Juroshek, „A direct calibration method for measuring equivalent source mismatch“, Microwave Journal, October 1997

VNA



If only  $\Gamma_{Eq}$  is needed

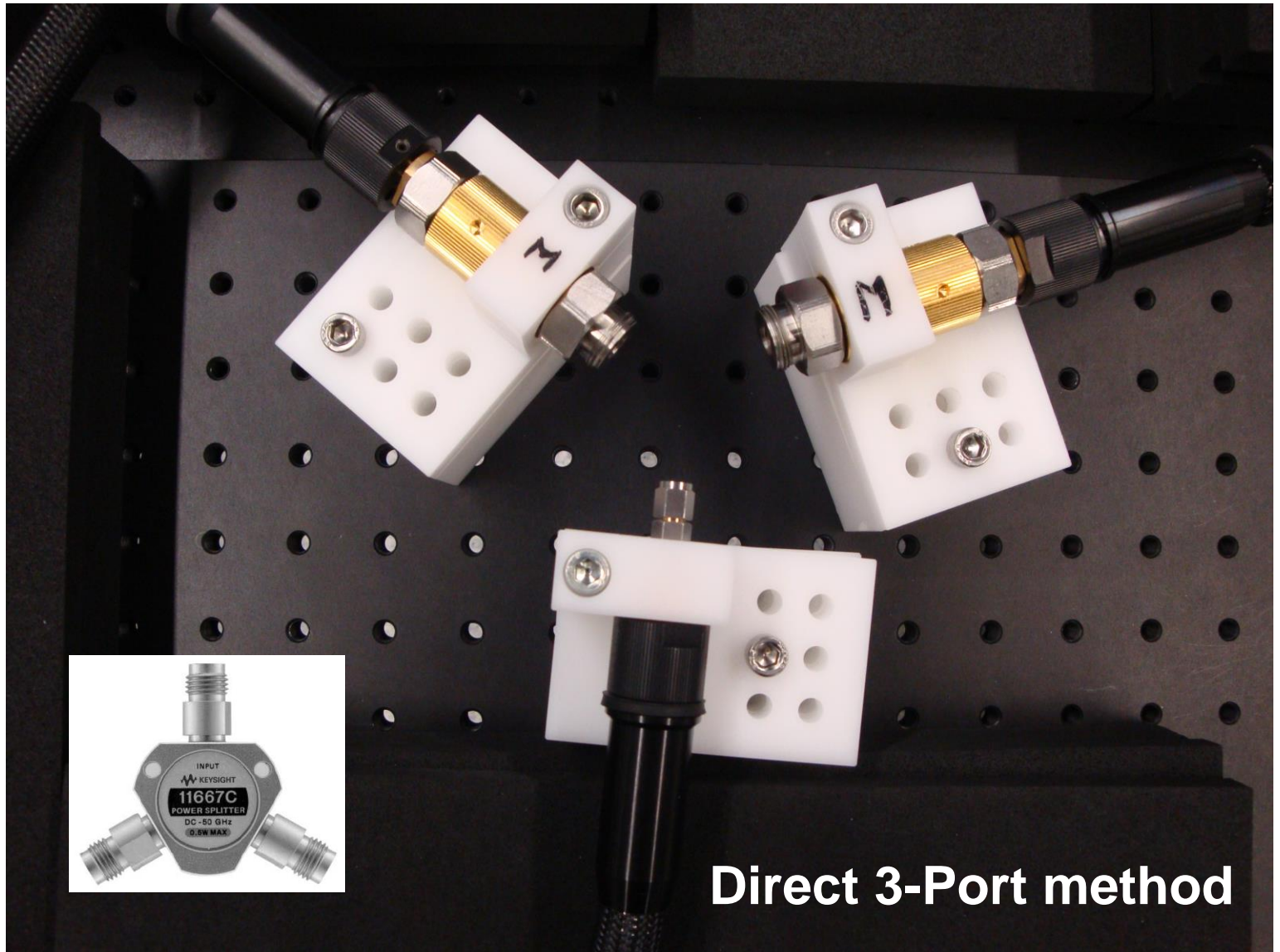


- Perform a OnePort calibration using the converted S-parameters

$$J_{33} = \frac{S_{11}}{S_{21}}$$

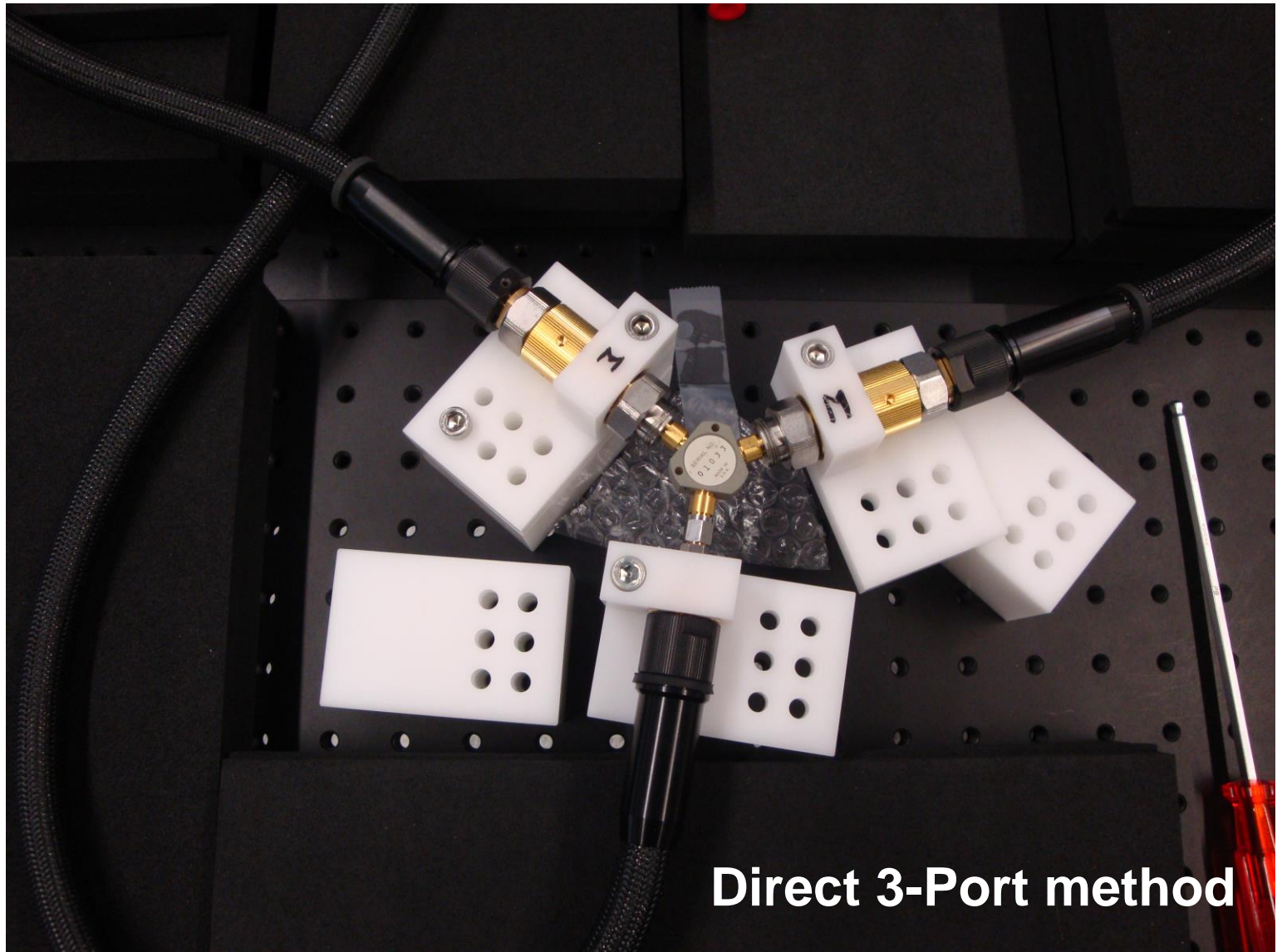
- Equivalent source match  $\Gamma_{Eq3}$ :  
-> equals the VNA source match
- Ratio of two VNA receiver ratios: thus the resulting directivity is the added directivity of both ports plus attenuation of the splitter.
- Mainly dependant on the accuracy of the Open and Short calibration standard definitions.
- Demands on noise and linearity of the VNA.

## 2.4 mm splitter setup using a 4-port VNA

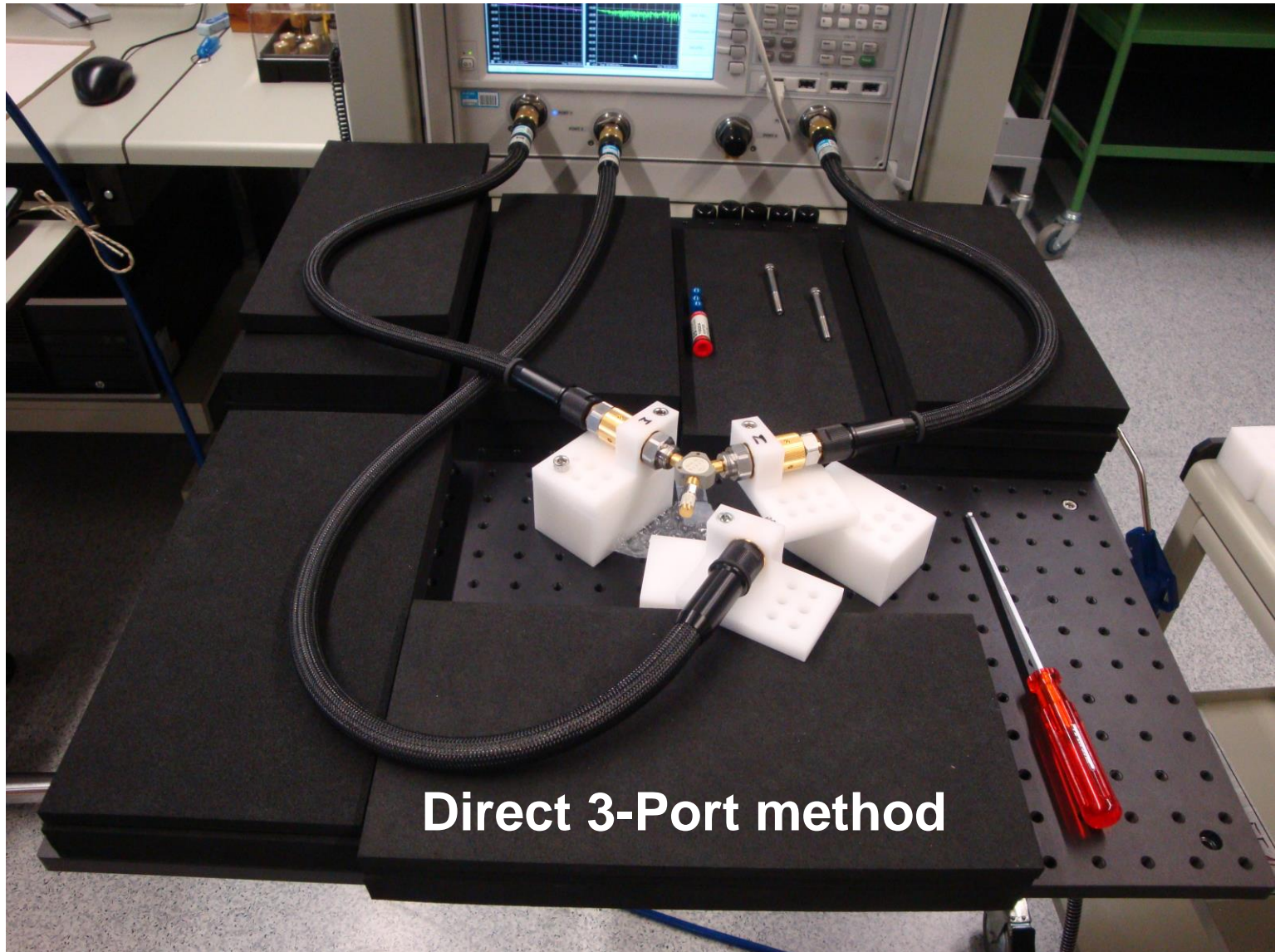




## 2.4 mm splitter setup using a 4-port VNA

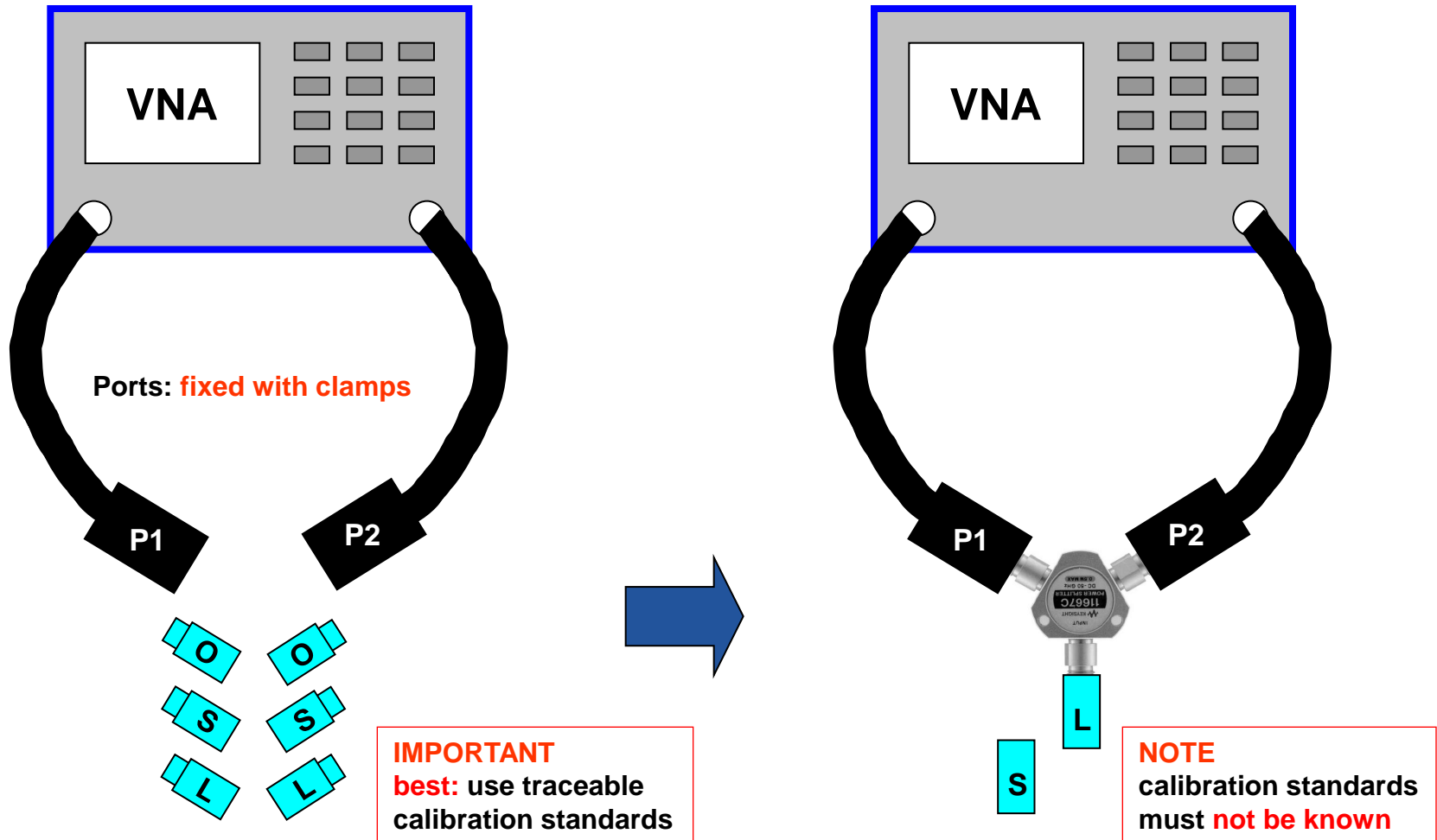


## 2.4 mm splitter setup using a 4-port VNA



# 2-Port “Palmer” VNA measurement method

## how to minimize the cable movement effects?

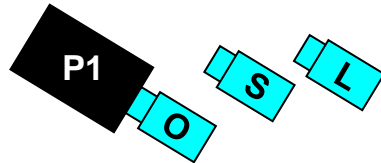




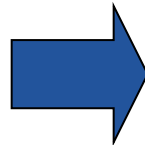
# 2-Port setup introducing the least cable effects

## 1st step: calibration on P1

Port 1: **fixed with a clamp**



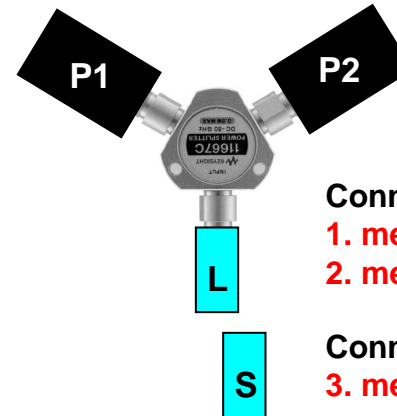
Measure Open, Short, Load on P1:  
 - **measure S11 only**  
 - **best:** include the connector effects



## 2nd step: connect splitter outputs to P1 and P2

Port 1: **fixed**

Port 2: **free**



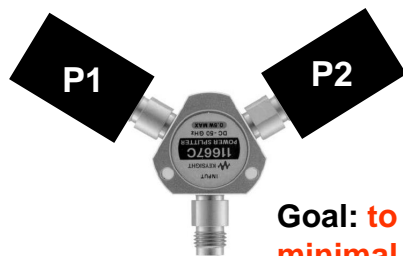
Connect a Load to the input port:  
 1. **measure all 4 S-parameters**  
 2. **measure the Switch Terms**

Connect a Short to the input port:  
 3. **measure all 4 S-parameters**

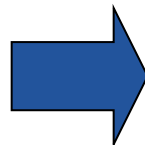
## 3rd step: first loose the P1 clamp, then fix P2 and remove the splitter

Port 1: **free**

Port 2: **fixed**

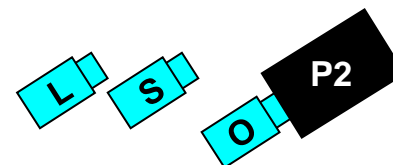


**Goal: to introduce minimal cable effects!**



## 4th step: calibration on P2

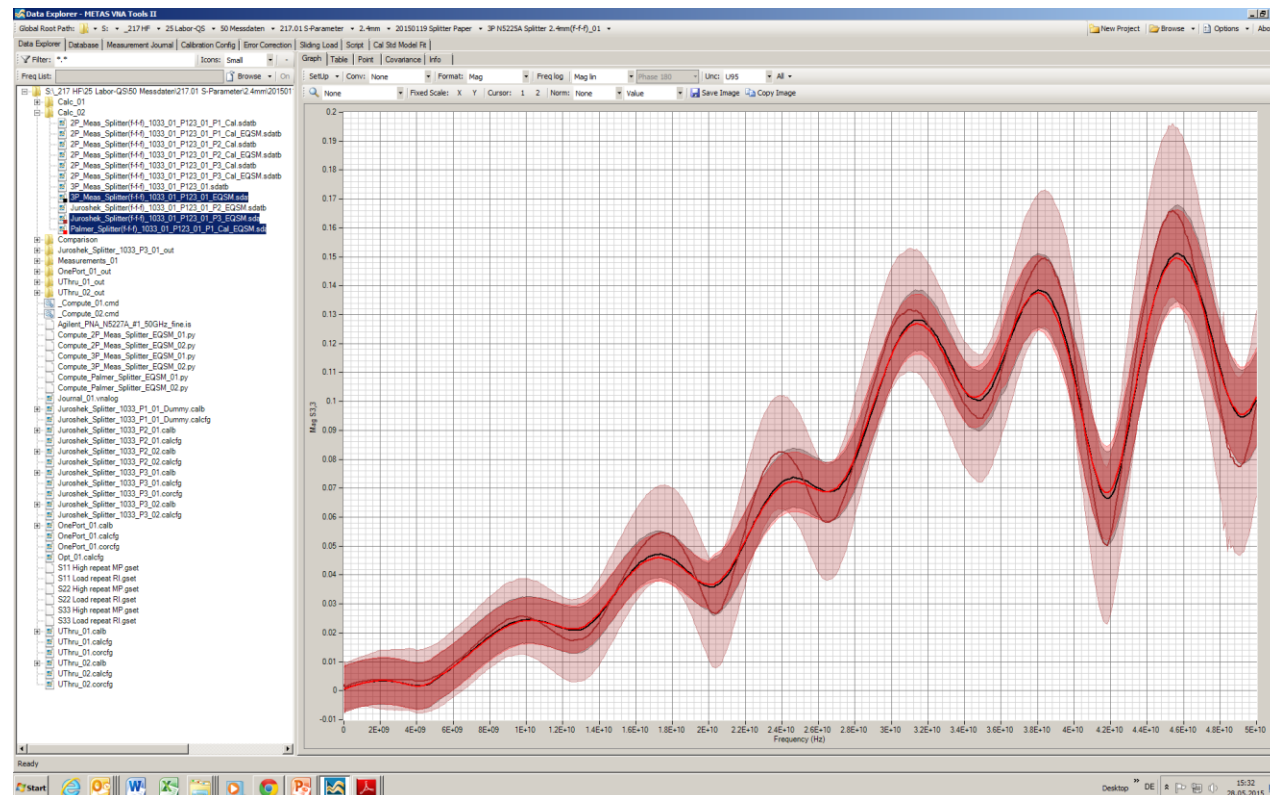
Port 2: **fixed with a clamp**



Measure Open, Short, Load on P2:  
 - **measure S22 only**  
 - **best:** include the connector effects

# VNA Tools

- VNA Tools II supports the Juroshek, 3-Port and 2-Port (using an unknown Load and Short) technique. All methods work with linear uncertainty propagation.



<http://www.metas.ch/vnatools>



# Conclusions

## splitter measurements at METAS

- **No need for an expensive 4-port VNA.**
- **Better invest the money for traceable calibration standard definitions** (including the systematic connector effects).
- **Each method has its pro and cons** (best: 2-Port “Palmer”).
- **Pre-select the power splitter for its repeatability behaviour.**
- **Avoid the unpredictable near field coupling effects:**  
**Use test port adapters showing a minimal pin-depth value.**





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Thank you very much for your attention

## References

- J. Hoffmann, M. Wollensack, J. Ruefenacht, M. Zeier, "Comparison of Methods for Measurement of Equivalent Source Match", 45th European Microwave Conference, EuMC 2015, Paper ID: EuMC40-01, September 2015.
- J. Hoffmann, K. Wong, "Improving VNA measurement accuracy by including connector effects in the models of calibration standards", Microwave Measurement Conference, 2013, 82nd ARFTG, pages 1-7.

A solid blue horizontal bar.

# Appendix

# Swap equal adapter method (non-insertable)



Step 1:



Forward Transmission:  $E_{TF}$   
Forward Match:  $E_{LF}$

Step 2:



Reverse Transmission:  $E_{TR}$   
Reverse Match:  $E_{LR}$

Step 3:



Forward Reflection Calibration  
**measures:**  $E_{DF}$ ,  $E_{SF}$ ,  $E_{RF}$   
using on P1: Open, Short, Load

Step 4:



Reverse Reflection Calibration  
**measures:**  $E_{DR}$ ,  $E_{SR}$ ,  $E_{RR}$   
using on P2: Open, Short, Load

Step 5:

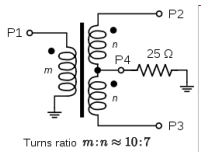


Device measurement  
**measures:**  $S_{11}$ ,  $S_{21}$  then reverse stimulus to **measure:**  $S_{22}$ ,  $S_{12}$

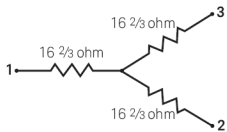
# Power splitter or divider

-> choose the right one (list not complete)

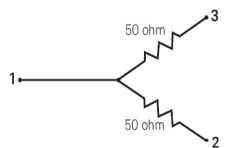
- **„Real“ 3 dB power divider:** hybrid type, realized with transformer circuits, only small loss (0.2 dB), no DC – response, high decoupling of the output ports, low to medium power applications, 0° or 90° phase types available.



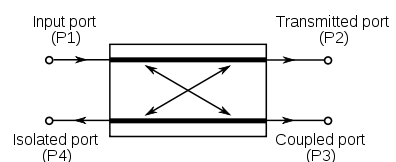
- **3-resistor divider (3 \* 16.7 Ω):** good match from DC to GHz, ideal e.g. for pulse signal / oscilloscope – applications, very high bandwidth, low decoupling between the output ports, low power applications.



- **2-resistor splitter (2 \* 50 Ω):** mainly used for ratio measurements and leveling applications, to maintain low source match ( $\Gamma_{Eq}$ ), very high bandwidth, low power applications.



- **3 dB directional coupler:** „real“ 3 dB power dividers (coupled transmission lines), band pass frequency response, very high power possible.



## Calculated minimal distances to avoid near field effects

based on the Agilent connector blue prints:

- **1.0 mm (slotted) : 5  $\mu\text{m}$**
- **1.85 mm (slotted) : 5  $\mu\text{m}$**
- **2.4 mm (slotless) : 15  $\mu\text{m}$**
- **2.92 mm (slotted) : 10  $\mu\text{m}$**
- **3.5 mm (slotless) : 15  $\mu\text{m}$**
- **Type-N (slotless) : 12  $\mu\text{m}$**

**General: a slotless design needs more distance!**